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Innovative Formulation in Discrete Kalman Filtering with Constraints - A Generic Framework for Comprehensive Error Analysis

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Abstract: This manuscript establishes a generic framework for comprehensive error analysis in discrete Kalman filtering with constraints, which systematically provides a complete set of algorithmic formulas along with demonstrating an alternative process of theoretical analytics of discrete Kalman filter. This constructive work aims extensively to standardize the formulation of Kalman filter with constraints. In analogy to the similar framework for standard discrete Kalman filter (without any constraints), the proposed framework specifically considers: model formulation vs. the error sources, the solution of the state and process noise vectors, the residuals for the process noise vector and the measurement noise vector. the redundancy contribution of the predicted state vector, process noise vector and measurement vector, and other relevant essential aspects, of which some of the features are essential to comprehensive error analysis, but are nonexistent yet in the primary algorithm in Kalman filtering with constraints. Besides, the algorithmic form of the Extended Kalman filter with constraints is also provided for practical purpose. At the end, specific remarks about the developed framework are given to emphasize on its usage to a certain extend.

KEY WORDS: Kalman filter, state constraint, error analysis, generic framework, redundancy contribution.

1. INTRODUCTION

The Kalman filter is a recursive estimator that provides estimates of a group of selected states on the ground of a specific system model and measurements that are acquired over time. Its applications have steadily expanded in sciences and engineering since the 1960s.

Usually, the Kalman filter consists of a system

model associated with its modeling errors as process noises and a measurement model associated with measurement noise. However, there are also many circumstances under which a priori knowledge of a dynamic system leads to equality constraints that may be imposed on the system states in Kalman filtering. Examples of this include pathconstrained motion along roadways [Yang et al, 2005; Hasberg et al 2012] and constant velocity motion of tracking targets [Alouani and Blair, 1991]. In multisensor integrated navigation, the states representing the attitude commonly involve specific constraints, e.g., the elements of the direction cosine matrix have to conform to orthonormality conditions and the elements in a quaternion vector or rotation vector have to be in unit norm. Apparently, the formulation of indirect observation (Least Squares) adjustment with constraints in Geodesy and Geomatics has been generally standardized [Mikhail, 1970; Rao and Toutenburg, 1999; Wang, et al, 2019]. By contrast, the formulation on states-constrained Kalman filter is far from being standardized to the same degree.

Constrained Kalman filtering by augmentation was first proven by Doran [1992], which has been considered as a seminal paper on the subject [Pizzinga, 2012]. There exist several dominant strategies to impose constraints on the system states in Kalman filtering, which are generally divided into three categories [Simon, 2010; Khabbazi and Esfanjani, 2014]:

<u>Reparameterization</u>: this technique incorporates any system state constraints by reducing the parameterization of the system, through which the physical meaning of the system states may be lost [Simon, 2010].

<u>"Perfect" Observations</u>: this technique treats the system state constraints as pseudo-observations with zero variance. Without further simplification, it may

cause numerical instability [Doran, 1992; Alouani and Blair, 1991].

Projection: this technique transforms the estimate of the system states onto a constraint surface [Khabbazi and Esfanjani, 2014]. Such transformation may be accomplished through projection of the system state estimate [Simon and Chia, 2002], projection of the system itself [Ko and Bitmead, 2007], or projection of the Kalman gain matrix [Teixeira et al, 2008]. State projection is the most commonly used method of imposing constraints on the system states in Kalman filtering [Khabbazi and Esfanjani, 2014]. The Kalman gain projection has been generalized for non-linear constraints [Xu et al, 2017]. These techniques may also apply their constraints less strictly by taking a weighted average between the constrained and the unconstrained solution [Baker and Thennadil, 2019], or by taking model uncertainty into account in the gain projection approach [Khabbazi and Esfanjani, 2015].

Besides, some other techniques have also been used to impose equality constraints in Kalman filtering that do not fit under the above mentioned three broad categories. Xu et al [2013] considered constraints *a priori* information that should also be incorporated into a system's dynamic models. Ghanbarpourasl and Zobar [2022] utilized singular value decomposition to separate the system state into a deterministic (i.e. fully constrained) and a stochastic component. Pizzinga [2012] framed the constrained Kalman filter as a recursive leastsquares problem.

Unfortunately, there is still a lack of generic algorithmic formulas directly for the standard form of the discrete Kalman filter with constraints in literature for conducting comprehensive error analysis. This motivates the authors to develop a complete set of the generic formulas for it, so that one can easily adapt to theoretical development and practical implementation.

Following this introduction, this manuscript first summarizes the innovative alternate formulation of standard Kalman filter originally deduced by Wang [1997] and also specifically detailed and applied in [Caspary and Wang, 1998; Wang, 1997; Wang, 2008, 2009; Wang et al, 2009; Wang et al, 2009; Gopaul et al, 2010; Wang et al, 2010; Oian, 2017; Qian, et al, 2015, 2016; Wang et al, 2015, 2021; Zhang et al, 2017]. Then, as the core of this manuscript, Section 3 systematically develops the theoretical aspects and practical algorithm in discrete Kalman filtering with constraints, which innovatively promote the comprehensive error analysis. Section 4 further delivers the proposed algorithm in the form of Extended Kalman filter with constraints. The manuscript ends with concluding remarks in Section 5.

2. ALGORITHMIC FORMULATIONS OF STANDARD KALMAN FILTER

In general, a Kalman filter estimates the state vector by minimizing its mean squared errors after the minimum variance principle or equivalently its weighted sum of the residuals squared after the Principle of Least Squares, on the basis of operating system and measurement models recursively.

2.1 Standard form of Discrete Kalman filter

Let us define the standard form of Kalman filter first. Consider a linear or linearized system described in state space and the data are made available over a discrete time series $t_0, t_1, \dots, t_k, \dots, t_N$, of which each time instant corresponds to an observation epoch and is simply depicted as $0, 1, \dots, k, \dots, N$. Without loss of generality, the formulation here omits the deterministic system input.

At an arbitrary observation epoch k ($1 \le k \le N$), the system and measurement models are given as follows [Wang et al, 2021]:

 $\mathbf{x}(k) = \mathbf{A}(k, k-1)\mathbf{x}(k-1) + \mathbf{B}(k, k-1)\mathbf{w}(k)$ (2.1)

(or simply x(k) = A(k)x(k-1) + B(k)w(k) (2.1a))

$$\boldsymbol{z}(k) = \boldsymbol{C}(k)\boldsymbol{x}(k) + \boldsymbol{\Delta}(k) \tag{2.2}$$

wherein $\mathbf{x}(k)$, $\mathbf{z}(k)$, $\mathbf{w}(k)$, and $\Delta(k)$ are the *n*dimensional state-vector, the *p*-dimensional observation vector, the *m*-dimensional process noise vector, and the *p*-dimensional measurement noise vector, respectively, while A(k, k-1), B(k, k-1), and C(k) are the $n \times n$ coefficient matrix of x(k), the $n \times m$ coefficient matrix of w(k), and the $p \times n$ coefficient matrix of z(k), respectively. relevant stochastic About the information, $w(k) \sim N(o, Q(k))$ and $\Delta(k) \sim N(o, R(k))$ are assumed, where N(a,b) represents a normal distribution with a and b as its expectation (vector) and variance (matrix). Between two different observation epochs, it is presumed to have Cov(w(i), w(j)) = 0 and $Cov(\Delta(i), \Delta(j)) = 0$ for $(i \neq j)$, and $Cov(w(i), \Delta(j)) = 0$ for any *i* and *j*.

Besides, the initial state vector is given as $\mathbf{x}(0)$ with its variance matrix $\mathbf{D}_{xx}(0)$ and is independent of $\mathbf{w}(k)$ and $\Delta(k)$ for any k, i.e., $Cov(\mathbf{w}(k))$, $\mathbf{x}(0) = \mathbf{0}$ and $Cov(\Delta(k), \mathbf{x}(0)) = \mathbf{0}$.

2.2 The Solution after Minimum Variance Principle

Without any unnecessary repetition of the solution derivation, the Kalman filtering algorithm at k from k-1 upon the definition in Section 2.1 after

the minimum variance principle is directly summarized below:

$$\hat{x}(k) = \hat{x}(k/k-1) + G(k)d(k)$$
 (2.3)

with its associated variance matrix

$$D_{xx}(k) = [I - G(k)C(k)]D_{xx}(k/k-1)$$

$$\cdot [I - G(k)C(k)]^{T} + G(k)R(k)G^{T}(k)$$
(2.4)

wherein I is a nxn identity matrix and G(k) is a nxp Kalman gain matrix:

$$\boldsymbol{G}(k) = \boldsymbol{D}_{xx}(k/k-1)\boldsymbol{C}^{T}(k)\boldsymbol{D}_{dd}^{-1}(k)$$
(2.5)

The predicted state vector (from the time update) and its variance matrix are as follows:

$$\hat{x}(k/k-1) = A(k)\hat{x}(k-1/k-1)$$
(2.6)

$$\boldsymbol{D}_{xx}(k/k-1) = \boldsymbol{A}(k)\boldsymbol{D}_{xx}(k-1/k-1)\boldsymbol{A}^{T}(k) + \boldsymbol{B}(k)\boldsymbol{Q}(k)\boldsymbol{B}^{T}(k)$$
(2.7)

The system innovation vector and its variance matrix are computed after:

$$d(k) = z(k) - C(k)\hat{x}(k/k-1)$$
(2.8)

$$\boldsymbol{D}_{dd}(k) = \boldsymbol{C}(k)\boldsymbol{D}_{xx}(k-1/k-1)\boldsymbol{C}^{T}(k) + \boldsymbol{R}(k) \quad (2.9)$$

Essentially, the system innovation vectors: d(1), d(2), ..., d(k), ... are independent of each other [Chui & Chen, 1987], i.e., Cov(d(i), d(j)) = O $(i \neq j)$. However, the elements in d(k) at epoch k are not only correlated, but also blend all of the separate error sources. Traditionally, the error analysis has been centered on the system innovation series. In addition, it is proved that the estimate of the state vector $\mathbf{x}(k)$ and the system innovation vector d(k) are independent of each other based on (2.3) and (2.8), i.e.,

$$\boldsymbol{D}_{xd}(k) = \boldsymbol{O} \tag{2.10}$$

2.3 Alternate Formulation for Comprehensive Error Analysis

Obviously, d(k) is originated from the process noise series w(1), ..., w(k), ..., the measurement noise series $\Delta(1), ..., \Delta(k), ...$ along with the initial state vector x(0). Therefore, as a matter of fact, the system and measurement models in (2.1) and (2.2) are associated with three groups of independent stochastic information that is propagated into the state solution from time to time. Specifically at k, the system is contaminated by (i) the measurement noise vector $\Delta(k)$, (ii) the process noise vector w(k), and (iii) the noise associated with the predicted state vector from A(k,k-1)x(k-1), into which $\Delta(1), ...,$ $\Delta(k-1)$ and w(1), ..., w(k-1) starting with x(0)are propagated through the recursive mechanism as in (2.1) and (2.2) from the past. Along two different paths, either after the Minimum Variance Principle or Least Squares Principle, the Kalman filtering algorithm is equivalently derived. A widely repeated derivation is to deliver the equivalent solution on the ground of the predicted state vector $\mathbf{x}(k/k-1)$, as a pseudomeasurement vector by merging (ii) and (iii) as in (2.1) in Least Squares approach, and the measurement vector $\mathbf{z}(k)$ from (i). An apparent drawback to this formulation is that two groups of the independent stochastic information in (ii) and (iii) are blended into $\mathbf{x}(k/k-1)$ and are no more separable in error analysis.

To enhance the error analysis in discrete Kalman filtering, Wang [1997] proposed an innovative alternate formulation. Innovatively, the system state prediction in (2.1) was further split into two pseudo-measurement vectors:

$$\boldsymbol{l}_{x}(k) = \boldsymbol{A}(k)\hat{\boldsymbol{x}}(k-1) = \hat{\boldsymbol{x}}(k/k-1) \quad \boldsymbol{D}_{l,l_{x}}(k) \quad (2.11)$$

$$\boldsymbol{l}_{w}(k) = \boldsymbol{w}_{0}(k) \qquad \qquad \boldsymbol{Q}(k) \qquad (2.12)$$

with $\boldsymbol{w}_0(k) = \boldsymbol{o}$ (zero mean presumed) and

$$\boldsymbol{D}_{l_x l_x}(k) = \boldsymbol{A}(k) \boldsymbol{D}_{xx}(k-1) \boldsymbol{A}^T(k)$$
(2.13)

The real measurement vector z(k) remains as in (2.2) and denoted by $l_z(k) = z(k)$.

The residual equations corresponding to (2.11), (2.12) and (2.2) are as follows:

$$\boldsymbol{v}_{l_x}(k) = \hat{\boldsymbol{x}}(k) - \boldsymbol{B}(k)\hat{\boldsymbol{w}}(k) - \boldsymbol{l}_x(k) \qquad (2.14)$$

$$\boldsymbol{v}_{\boldsymbol{l}_{w}}(k) = \hat{\boldsymbol{w}}(k) - \boldsymbol{l}_{w}(k) \quad (2.15)$$

$$\boldsymbol{v}_{\boldsymbol{l}_z}(k) = \boldsymbol{C}(k)\hat{\boldsymbol{x}}(k) \qquad -\boldsymbol{l}_z(k) \qquad (2.16)$$

with $D_{l_x l_x}(k)$, Q(k) and R(k) as their measurement variance matrices, respectively, in which the state vector is extended to include the process noise vector w(k) being estimated together with x(k).

In seeking for a Least Squares solution for x(k) and w(k), the cost function is constructed

$$\min: g(k) = \mathbf{v}_{l_{x}}^{T}(k) \mathbf{D}_{l_{x}l_{x}}^{-1}(k) \mathbf{v}_{l_{x}}(k) + \mathbf{v}_{l_{w}}^{T}(k) \mathbf{Q}^{-1}(k) \mathbf{v}_{l_{w}}(k) + \mathbf{v}_{z}^{T}(k) \mathbf{R}^{-1}(k) \mathbf{v}_{z}(k)$$
(2.17)

In (2.14), (2.15) and (2.16), there are (n + m) states and (n + m + p) measurements. The number of the redundant measurements remains unchanged, namely, *p*. It is not in question about the identity of $\mathbf{x}(k)$ derived after (2.17) and the one in (2.3) [Wang, 1997]. The beauty of this formulation lies in the feasibility for the direct analysis of the three original error sources at any epoch *k*. Especially, it allows for reliability analysis in discrete Kalman filtering [Wang, 1997, 2009]. For the benefit of the presentation in next section, the outcome from this alternate formulation is summarized below:

1) The solution of the state vector

First, equations (2.3) - (2.9) in Section 2.2 remain unchanged to form the basis of the solution. Alternatively, (2.3) is also given as follows

$$\begin{aligned} \mathbf{x}(k/k) &= \mathbf{l}_{x}(k) + \mathbf{B}(k)\mathbf{l}_{w}(k) \\ &+ \mathbf{K}(k)\{\mathbf{l}_{z}(k) - \mathbf{C}(k)[\mathbf{l}_{x}(k) - \mathbf{B}(k)\mathbf{l}_{w}(k)]\} \end{aligned}$$
(2.18)

Importantly, the process noise vector is estimated by

$$\hat{\boldsymbol{w}}(k) = \boldsymbol{w}_0(k)$$

$$+ \boldsymbol{Q}(k) \boldsymbol{B}^T(k) \boldsymbol{D}_{vv}^{-1}(k/k-1) \boldsymbol{K}(k) \boldsymbol{d}(k)$$
(2.19)

with its variance matrix

$$D_{ww}(k) = Q(k)$$

$$-Q(k)B^{T}(k)C^{T}(k)D_{dd}^{-1}(k)C(k)B(k)Q(k)$$
(2.20)

and its covariance matrix with the estimated state vector

$$D_{xw}(k) = B(k)Q(k)$$

- $D_{xx}(k/k-1)C^{T}(k)D_{dd}^{-1}(k)C(k)B(k)Q(k)$ (2.21)

2) The residual vectors

$$v_{l_x}(k) = D_{l_y l_y}(k) D_{xx}^{-1}(k/k-1) G(k) d(k)$$
 (2.22)

$$\boldsymbol{v}_{w}(k) = \boldsymbol{Q}(k)\boldsymbol{B}^{T}(k)\boldsymbol{D}_{xx}^{-1}(k/k-1)\boldsymbol{G}(k)\boldsymbol{d}(k) \qquad (2.23)$$

$$\boldsymbol{v}_{\tau}(k) = [\boldsymbol{C}(k)\boldsymbol{G}(k) - \boldsymbol{I}]\boldsymbol{d}(k)$$
(2.24)

with *their variance matrices*

$$\boldsymbol{D}_{\boldsymbol{v}_{L},\boldsymbol{v}_{L}}(k) = \boldsymbol{D}_{l_{r}l_{r}}(k)\boldsymbol{C}^{T}(k)\boldsymbol{D}_{dd}^{-1}(k-1)\boldsymbol{C}(k)\boldsymbol{D}_{l_{r}l_{r}}(k) \quad (2.25)$$

$$\boldsymbol{D}_{\boldsymbol{\nu}_{w},\boldsymbol{\nu}_{w}}(k) = \boldsymbol{Q}(k)\boldsymbol{B}^{T}(k)\boldsymbol{C}^{T}(k)\boldsymbol{D}_{dd}^{-1}(k)\boldsymbol{C}(k)\boldsymbol{B}(k)\boldsymbol{Q}(k) \quad (2.26)$$

$$\boldsymbol{D}_{\boldsymbol{k},\boldsymbol{k}}(k) = [\boldsymbol{I} - \boldsymbol{C}(k)\boldsymbol{G}(k)]\boldsymbol{R}(k)$$
(2.27)

3) *The redundancy contributions* in measurement groups corresponding to (2.11), (2.12) and 2.2):

$$r_{l_x}(k) = tr[A(k)D_{xx}(k-1)A^{T}(k)C^{T}(k)D_{dd}^{-1}(k)C(k)] (2.28)$$

$$r_{l_w}(k) = tr[\boldsymbol{Q}(k)\boldsymbol{B}^T(k)\boldsymbol{C}^T(k)\boldsymbol{D}_{dd}^{-1}(k-1)\boldsymbol{C}(k)\boldsymbol{B}(k) \quad (2.29)$$

$$r_{z}(k) = tr[I - C(k)G(k)]$$
(2.30)

For the entire system either after (2.1) and (2.2), or after (2.11), (2.12) and (2.2), the total redundancy number at epoch k satisfies [Wang, 1997; 2009, 2021; etc]

$$r(k) = r_{l_x}(k) + r_{l_w}(k) + r_z(k) = p(k)$$
(2.31)

wherein p(k) is the number of the real measurements or the dimension of z(k).

4) The individual redundancy indexes

In practice, Q(k) and R(k) are commonly diagonal so that the individual redundancy indexes in components for the process noise vector are

$$r_{w_i}(k) = [\boldsymbol{Q}(k)\boldsymbol{B}^T(k)\boldsymbol{C}^T(k)\boldsymbol{D}_{dd}^{-1}(k)\boldsymbol{C}(k)\boldsymbol{B}(k)]_{ii}$$

$$(i = 1, 2, ..., m(k))$$
 (2.32)

and for the measurement vector

$$r_{z_i}(k) = [I - C(k)G(k)]_{ii} \quad (i = 1, 2, ..., p(k)) \quad (2.33)$$

Indeed, as $D_{l_x l_x}(k)$ in (2.11) is not a diagonal matrix in general, no individual redundancy indexes in components become meaningful here for $l_x(k)$.

5) The variance of unit weight (the variance factor)

$$\hat{\sigma}_0^2(k) = d^T(k)D_{dd}^{-1}(k)d(k)/p(k)$$
 (2.34)

or

$$\hat{\sigma}_{0}^{2}(k) = [\mathbf{v}_{l_{x}}^{T}(k)\mathbf{D}_{l_{x}l_{x}}^{-1}(k)\mathbf{v}_{l_{x}}(k) + \mathbf{v}_{l_{w}}^{T}(k)\mathbf{Q}^{-1}(k)\mathbf{v}_{l_{w}}(k) + \mathbf{v}_{z}^{T}(k)\mathbf{R}^{-1}(k)\mathbf{v}_{z}(k)]/p(k)$$
(2.35)

6) *The posteriori variance matrix* of the estimated state vector

$$\hat{\boldsymbol{D}}_{xx}(k) = \hat{\sigma}_0^2(k) \boldsymbol{D}_{xx}(k)$$
(2.36)

which directly reflects the latest available residuals due to the modeling and measurement errors. For the usage in (2.36), one can apply the epochwise variance factor as in (2.34) or (2.35), a regional variance factor, i.e., an average over a specific time period, or even a global variance factor from the entire data period [Wang, 1997, 2009; Wang et al, 2021]. However, it is noticed that plenty of the applications with applying Kalman filter have inappropriately considered (2.4), instead of (2.36), as their posteriori state variance matrix.

Refer to [Wang, 1997, 2008, 2009; Caspary and Wang, 1998; Wang et al, 2021] for more details about this alternate formulation and its advantages for error analysis in discrete Kalman filtering.

3. GENERIC FORMULATION OF DISCRETE KALMAN FILTER WITH CONSTRAINTS

This section provides readers with our original development of a generic formula set, which meaningfully serves as an innovative framework for comprehensive error analysis in discrete Kalman filtering with constraints in parallel with the one summarized in Section 2.3, and also describes their connections. In this work, the constraints are restricted to the equality constraints,

3.1 The Functional and Stochastic Models

Upon the models of the standard Kalman filter defined in Section 2.1, a Kalman filter with constraints indicates that there exist the following additional constraints among the states

$$\boldsymbol{H}^{T}(\boldsymbol{k})\boldsymbol{x}(\boldsymbol{k}) - \boldsymbol{h} = \boldsymbol{o} \tag{3.1}$$

wherein H(k) is a *n*×*h*-dimensional coefficient matrix and tr[H(k)] = h (h < n), which is either originally linear or linearized from nonlinear constraints and **h** is the *h*-dimensional constant vector. Hence, the equations (2.1), (2.2) and (3.1) together represent the system model, the measurement model, and the constraints among the states in discrete Kalman filtering.

In analogy to the alternate formulation summarized in Section 2.3, the Principle of Least Squares is straightforwardly applied epochwise hereinafter to result the solution for discrete Kalman filter with constraints. To demonstrate the flexibility in dealing with the available functional and stochastic models, three different ways that deliver an identical estimate of the state vector $\mathbf{x}(k)$ are introduced in Sections 3.2, 3.3 and 3.4, respectively, of which Section 3.4 is the focus of attention of this manuscript.

3.2 Approach One

The measurement equation system is here structured as follows

1) *a pseudo-measurement vector* $l'_x(k)$ is given directly by using the solution of the state vector from the standard Kalman filter (without any constraints) as in Section 2, which establishes the following residual equation:

$$\boldsymbol{v}_{x}(k) = \boldsymbol{x}_{h}(k) - \boldsymbol{l}_{x}'(k) \tag{3.2}$$

wherein $\mathbf{x}_h(k)$ is the state estimate subject to the constraints as in (3.1) while the pseudomeasurement vector and its variance matrix are:

$$l'_{x}(k) = x(k/k)$$
 (refer to (2.3)) (3.3)

$$D_{l'_{x}l'_{x}}(k) = D_{xx}(k)$$
 (refer to (2.4)) (3.4)

2) *a group of h linear constraints* as in (3.1) are applied.

The equations (3.2) and (3.1) together compose the model in the form of indirect observations with constraints. So, the Principle of Least Squares is applied to the following cost function at epoch *k*:

$$\min : g(\boldsymbol{x}_{h}(k)/\boldsymbol{l}'_{x}(k), \boldsymbol{z}(k)) = v_{\boldsymbol{l}'_{x}}^{T}(k)\boldsymbol{D}_{\boldsymbol{l}'_{x}\boldsymbol{l}'_{x}}^{-1}(k)\boldsymbol{v}_{\boldsymbol{l}'_{x}}(k) + 2\boldsymbol{k}_{h}^{T}[\boldsymbol{H}^{T}(k)\boldsymbol{x}_{h}(k) - \boldsymbol{h}]$$
(3.5)

which was called the Mean Square Method in [Simon and Chia, 2000]. To seek for the (minimum) extreme value of (3.5), its first order derivative with respect to $\boldsymbol{x}_{h}(k)$ is assigned to 0:

$$\frac{\partial}{\partial \boldsymbol{x}_{h}(k)} g(\boldsymbol{x}_{h}(k) / \boldsymbol{l}_{x}'(k), \boldsymbol{z}(k))$$

= $2\boldsymbol{v}_{\boldsymbol{l}_{x}}^{T}(k)\boldsymbol{D}_{xx}^{-1}(k/k) + 2\boldsymbol{k}_{h}^{T}\boldsymbol{H}^{T}(k) = \boldsymbol{o}$ (3.6)

which yields

$$\boldsymbol{D}_{xx}^{-1}(k)\boldsymbol{x}_{h}(k) + \boldsymbol{H}(k)\boldsymbol{k}_{h}(k) - \boldsymbol{D}_{xx}^{-1}(k)\boldsymbol{l}_{x}'(k) = \boldsymbol{o} \quad (3.7)$$

The equations (3.7) and (3.1) together compose a normal equation system:

$$\begin{pmatrix} \boldsymbol{D}_{xx}^{-1}(k/k) & \boldsymbol{H}(k) \\ \boldsymbol{H}^{T}(k) & \boldsymbol{O} \end{pmatrix} \begin{pmatrix} \boldsymbol{x}_{h}(k) \\ \boldsymbol{k}_{h} \end{pmatrix} = \begin{pmatrix} \boldsymbol{D}_{xx}^{-1}(k/k)\boldsymbol{l}_{x}'(k) \\ \boldsymbol{h} \end{pmatrix}$$
(3.8)

which possesses two unknown parameter vectors: the state vector $\mathbf{x}_h(k)$ and the Lagrange multiplier vector $\mathbf{k}_h(k)$ brought by the constraints.

To solve (3.8), one can first derive $\boldsymbol{x}_h(k)$ from the first equation:

$$\mathbf{x}_{h}(k) = \mathbf{D}_{xx}(k) [\mathbf{D}_{xx}^{-1}(k/k) \mathbf{l}'_{x}(k) - \mathbf{H}(k) \mathbf{k}_{h}(k)]$$

= $\mathbf{x}(k/k) - \mathbf{D}_{xx}(k/k) \mathbf{H}(k) \mathbf{k}_{h}(k)$ (3.9)

wherein $\mathbf{x}(k/k)$ is the minimum variance estimate of the state vector given in (2.3). Substituting (3.9) into the second equation of (3.8) delivers the Lagrange multiplier vector $\mathbf{k}_{h}(k)$:

$$\boldsymbol{k}_{h}(k) = \boldsymbol{N}_{hh}^{-1}(k) [\boldsymbol{H}^{T}(k)\boldsymbol{x}(k/k) - \boldsymbol{h}]$$
(3.10)

where a helping matrix $N_{hh}(k)$ is defined to simplify the notation

$$\boldsymbol{N}_{hh}(k) = \boldsymbol{H}^{T}(k)\boldsymbol{D}_{xx}(k/k)\boldsymbol{H}(k)$$
(3.11)

The substitution of (3.10) into (3.9) gives $x_h(k)$

$$\hat{\boldsymbol{x}}_{h}(k) = \boldsymbol{x}(k/k) - \boldsymbol{D}_{xx}(k/k)\boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)\{\boldsymbol{H}^{T}(k)\boldsymbol{x}(k/k) - \boldsymbol{h}\}$$
(3.12)

in which the overhead symbol ^ is commonly ignored wherever no confusion may occur.

The associated variance matrix with $x_h(k)$ is derived based on (3.12):

$$D_{x_h x_h}(k) = D_{xx}(k/k)$$

- $D_{xx}(k/k)H(k)N_{hh}^{-1}(k)H^T(k)D_{xx}(k/k)$ (3.13)

wherein $D_{xx}(k/k)$ is the variance matrix of x(k/k) in (2.4).

This solution is indeed identical with the one after Maximum Probability Method and Projection Method presented in Simon and Chia [2000].

3.3 Approach Two

Differently from Approach One in Section 3.2, the measurement equation system is here structured as follows

 A pseudo-measurement vector lⁿ_x(k) is defined by the predicted state vector x(k/k−1) from t_{k-1} to t_k (i.e., time update) from the standard

Kalman filter as in Section 2, which establishes the following residual equation:

$$v_{l_{x}'}(k) = x_{h}(k) - l_{x}''(k)$$
(3.14)

with

$$l''_{x}(k) = x(k/k-1) = A(k)x(k-1)$$
(3.15)

$$D_{I_{xx}''}(k) = D_{xx}(k/k-1)$$

= $A(k)D_{xx}(k-1)A^{T}(k) + B(k)Q(k)B^{T}(k)$ (3.16)

2) A measurement vector $l_z(k)$ is adapted from the real measurement vector z(k) at t_k as in (2.2), which yields the following residual equation:

$$\boldsymbol{v}_{l_z}(k) = \boldsymbol{v}_z(k) = \boldsymbol{C}(k)\boldsymbol{x}_h(k) - \boldsymbol{l}_z(k)$$
(3.17)

with

$$\boldsymbol{l}_{\boldsymbol{z}}(k) = \boldsymbol{z}(k) \tag{3.18}$$

$$\boldsymbol{D}_{l_z l_z}(k) = \boldsymbol{R}(k) \tag{3.19}$$

wherein C(k) is the same as in (2.2).

a group of h linear constraints as in (3.1) are applied, wherein h (bold and *italic*) is the constant vector in the constraints.

Now, the equations (3.14), (3.17) and (3.1) together compose another model in the form of indirect observations with constraints at epoch *k*. Accordingly, the cost function for applying the Principle of Least Squares is as below:

min:
$$g(\mathbf{x}_{h}(k)/l_{x}''(k), z(k))$$

= $\mathbf{v}_{l_{x}'}^{T}(k)\mathbf{D}_{l_{x}'l_{x}'}^{-1}(k)\mathbf{v}_{l_{x}'}(k) + \mathbf{v}_{l_{z}}^{T}(k)\mathbf{R}^{-1}(k)\mathbf{v}_{l_{z}}(k)$
+ $2\mathbf{k}_{h}^{T}(k)[\mathbf{H}^{T}(k)\mathbf{x}_{h}(k) - \mathbf{h}(k)]$ (3.20)

The same as with (3.5), the 1st order derivative of (3.20) with respect to $\boldsymbol{x}(k)$ is assigned to 0:

$$\frac{\partial}{\partial \boldsymbol{x}_{h}(k)} g(\boldsymbol{x}_{h}(k)/\boldsymbol{l}_{x}^{"}(k), \boldsymbol{z}(k)) = 2\boldsymbol{v}_{\boldsymbol{l}_{x}^{T}}^{T}(k)\boldsymbol{D}_{\boldsymbol{l}_{x}^{T}\boldsymbol{l}_{x}^{T}}^{-1}(k) + 2\boldsymbol{v}_{\boldsymbol{l}_{z}}^{T}(k)\boldsymbol{R}^{-1}(k)\boldsymbol{C}(k) + 2\boldsymbol{k}_{h}^{T}\boldsymbol{H}^{T}(k) = \boldsymbol{o}$$
(3.21)

which gives

$$\{\boldsymbol{D}_{l_{x}l_{x}}^{-1}(k) + \boldsymbol{C}^{T}(k)\boldsymbol{R}^{-1}(k)\boldsymbol{C}(k)\}\boldsymbol{x}_{h}(k) + \boldsymbol{H}(k)\boldsymbol{k}_{h} (3.22) - \boldsymbol{D}_{l_{x}l_{x}}^{-1}(k)\boldsymbol{l}_{x}(k) - \boldsymbol{C}^{T}(k)\boldsymbol{R}^{-1}(k)\boldsymbol{z}(k) = \boldsymbol{o}$$

From (3.22) and (3.1), the normal equation system goes as follows:

$$\begin{pmatrix} \boldsymbol{D}_{\boldsymbol{l}_{x}^{\prime}\boldsymbol{l}_{x}^{\prime\prime}}^{-1}(k) + \boldsymbol{C}^{T}(k)\boldsymbol{R}^{-1}(k)\boldsymbol{C}(k) & \boldsymbol{H}(k) \\ \boldsymbol{H}^{T}(k) & \boldsymbol{O} \end{pmatrix} \begin{pmatrix} \boldsymbol{x}_{h}(k) \\ \boldsymbol{k}_{h} \end{pmatrix} (3.23)$$
$$= \begin{pmatrix} \boldsymbol{D}_{\boldsymbol{l}_{x}^{\prime}\boldsymbol{l}_{x}^{\prime\prime}}^{-1}(k)\boldsymbol{l}_{x}^{\prime\prime}(k) + \boldsymbol{C}^{T}(k)\boldsymbol{R}^{-1}(k)\boldsymbol{z}(k) \\ \boldsymbol{h} \end{pmatrix}$$

which is identical to (3.8) because it can be proved

$$[\boldsymbol{D}_{l_x^{\prime} l_x^{\prime\prime}}^{-1}(k) + \boldsymbol{C}^T(k) \boldsymbol{R}^{-1}(k) \boldsymbol{C}(k)]^{-1} = \boldsymbol{D}_{xx}(k/k) \quad (3.24)$$

and

$$D_{l_{xt}''x}^{-1}(k)l_{x}''(k) + C^{T}(k)R^{-1}(k)z(k)$$

= $D_{xx}^{-1}(k/k-1)x(k/k-1) + C^{T}(k)R^{-1}(k)z(k)$ (3.25)
= $D_{xx}^{-1}(k)x(k)$

This implies that (3.8) and (3.23) result in the identical solution for the state vector.

3.4 Approach Three

Furthermore, differently from Approaches One and Two, Approach Three here develops the proposed framework for comprehensive error analysis in discrete Kalman filtering with constraints, which is particularly an extension of (2.14) - (2.16)by adding the constraints among the states. The measurement equation system is hereto structured as follows:

1) The first pseudo-measurement vector $l_x(k)$ is here defined by the predicted state vector exclusive of the effect of the process noise vector. Its residual equation is (refer to (2.14):

$$\mathbf{v}_{l_x}(k) = \mathbf{x}_h(k) - \mathbf{B}(k)\mathbf{w}_h(k) - \mathbf{l}_x(k)$$
(3.25)

$$l_{x}(k) = A(k)x(k-1)$$
(3.26)

$$\boldsymbol{D}_{l_{x}l_{x}}(k) = \boldsymbol{A}(k)\boldsymbol{D}_{xx}(k-1)\boldsymbol{A}^{T}(k)$$
(3.27)

2) *The second pseudo-measurement vector* $l_w(k)$ is defined by the process noise vector, which gives the residual equation below (refer to (2.15):

$$\boldsymbol{v}_{\boldsymbol{l}_{w}}(k) = \boldsymbol{w}_{h}(k) - \boldsymbol{l}_{w}(k) \tag{3.28}$$

$$l_{w}(k) = w_{0}(k)$$
 (usually $w_{0}(k) = o$) (3.29)

$$\boldsymbol{D}_{l_{w}l_{w}}(k) = \boldsymbol{Q}(k) \tag{3.30}$$

3) A measurement vector $l_z(k)$ is adapted from the

real measurement vector z(k) at t_k as in (2.2). So, the residual equation is as (3.17) alongside with (3.18) and (3.19).

4) a group of *h* linear or linearized constraints are as in (3.1).

Essentially, one must give one's attention to (3.26), $l_x(k) \neq x(k/k-1)$ because

$$\mathbf{x}(k/k-1) = \mathbf{l}_{\mathbf{x}}(k) + \mathbf{B}(k)\mathbf{l}_{w}(k)$$

= $\mathbf{A}(k)\mathbf{x}(k-1) + \mathbf{B}(k)\mathbf{w}_{0}(k)$ (3.31)

Writing four equations (3.25), (3.28), (3.17), and (3.1) together gives the entire residual equation system with constraints as below:

$$\begin{pmatrix} \mathbf{v}_{x}^{h}(k) \\ \mathbf{v}_{w}^{h}(k) \\ \mathbf{v}_{z}^{h}(k) \end{pmatrix} = \begin{pmatrix} \mathbf{E}_{x} & -\mathbf{B}(k) \\ \mathbf{O} & \mathbf{E}_{w} \\ \mathbf{C}(k) & \mathbf{O} \end{pmatrix} \begin{pmatrix} \mathbf{x}_{h}(k) \\ \mathbf{w}_{h}(k) \end{pmatrix} - \begin{pmatrix} \mathbf{I}_{x}(k) \\ \mathbf{I}_{w}(k) \\ \mathbf{I}_{z}(k) \end{pmatrix} (3.32)$$
$$\mathbf{H}^{T}(k)\mathbf{x}_{h}(k) - \mathbf{h} = \mathbf{O}$$

alongside with the blockwise covariance matrix of three independent measurement vectors $l_x(k)$, $l_w(k)$ and z(k) as in (3.27), (3.30), (3.19). The main difference of (3.32) from Approach One in

Section 3.2 and Approach Two in Section 3.3 lies in

directly modeling three originally independent random vectors as the measurement vectors. Accordingly, the unknown parameters have been extended from $\boldsymbol{x}_h(k)$ to both of $\boldsymbol{x}_h(k)$ and $\boldsymbol{w}_h(k)$, This modeling strategy allows estimating the process noise vector epochwise and also the residual vector of $\boldsymbol{l}_w(k)$, which has been of scarcely any mention in literature, except initially modeled in Wang [1997].

Frankly, (3.32) allows specifying the following cost function for applying the Principle of Least Squares:

$$\min : g(\mathbf{x}_{h}(k), \mathbf{w}_{h}(k) / l_{x}(k), l_{w}(k), l_{z}(k)) = \mathbf{v}_{l_{x}}^{T}(k) \mathbf{D}_{l_{x}l_{x}}^{-1}(k) \mathbf{v}_{l_{x}}(k) + \mathbf{v}_{l_{w}}^{T}(k) \mathbf{Q}^{-1}(k) \mathbf{v}_{l_{w}}(k) + \mathbf{v}_{l_{z}}^{T}(k) \mathbf{R}^{-1}(k) \mathbf{v}_{l_{z}}(k) + 2\mathbf{k}_{h}^{T}(k) [\mathbf{H}^{T}(k) \mathbf{x}_{h}(k) - \mathbf{h}(k)]$$
(3.33)

which yields two 1st order partial derivatives for $\boldsymbol{x}_h(k)$ and $\boldsymbol{w}_h(k)$, respectively:

$$\frac{\partial g(\boldsymbol{x}_{h}(k), \boldsymbol{w}_{h}(k) / \boldsymbol{l}_{\boldsymbol{x}}(k), \boldsymbol{l}_{w}(k), \boldsymbol{l}_{z}(k))}{\partial \boldsymbol{x}_{h}(k)}$$

$$= 2\boldsymbol{v}_{l_{\boldsymbol{x}}}^{T}(k)\boldsymbol{D}_{l_{\boldsymbol{x}}l_{\boldsymbol{x}}}^{-1}(k)$$

$$+ 2\boldsymbol{v}_{l_{\boldsymbol{x}}}^{T}(k)\boldsymbol{R}^{-1}(k)\boldsymbol{C}(k) + 2\boldsymbol{k}_{h}^{T}(k)\boldsymbol{H}^{T}(k) = \boldsymbol{o}$$
(3.34)

$$\frac{\partial g(\boldsymbol{x}_{h}(k), \boldsymbol{w}_{h}(k) / \boldsymbol{l}_{x}(k), \boldsymbol{l}_{w}(k), \boldsymbol{l}_{z}(k))}{\partial \boldsymbol{w}(k)}$$

$$= -2\boldsymbol{v}_{l_{x}}^{T}(k)\boldsymbol{D}_{l_{x}l_{x}}^{-1}(k)\boldsymbol{B}(k) + 2\boldsymbol{v}_{l_{w}}^{T}(k)\boldsymbol{Q}^{-1}(k) = \boldsymbol{o}$$
(3.35)

Together with (3.1), (3.34) and (3.35) build up the corresponding normal equation system:

$$\begin{pmatrix} \boldsymbol{D}_{l_{x}l_{x}}^{-1}(k) + \boldsymbol{C}^{T}(k)\boldsymbol{R}^{-1}(k)\boldsymbol{C}(k) & -\boldsymbol{D}_{l_{x}l_{x}}^{-1}(k)\boldsymbol{B}(k) & \boldsymbol{H}(k) \\ -\boldsymbol{B}^{T}(k)\boldsymbol{D}_{l_{x}l_{x}}^{-1}(k) & \boldsymbol{B}^{T}(k)\boldsymbol{D}_{l_{x}l_{x}}^{-1}(k)\boldsymbol{B}(k) + \boldsymbol{Q}^{-1}(k) & \boldsymbol{O} \\ \boldsymbol{H}^{T}(k) & \boldsymbol{O} & \boldsymbol{O} \end{pmatrix} \\ \cdot \begin{pmatrix} \boldsymbol{x}_{h}(k) \\ \boldsymbol{w}_{h}(k) \\ \boldsymbol{k}_{h}(k) \end{pmatrix} = \begin{pmatrix} \boldsymbol{D}_{l_{x}l_{x}}^{-1}(k)\boldsymbol{l}_{x}(k) + \boldsymbol{C}^{T}(k)\boldsymbol{R}^{-1}(k)\boldsymbol{l}_{z}(k) \\ -\boldsymbol{B}^{T}(k)\boldsymbol{D}_{l_{x}l_{x}}^{-1}(k)\boldsymbol{l}_{x}(k) + \boldsymbol{Q}^{-1}(k)\boldsymbol{l}_{w}(k) \\ \boldsymbol{h}(k) \end{pmatrix}$$
(3.36)

Although deducing an explicit solution of (3.36) affirmatively seems complicated because the coefficient matrix of (3.36) is in the form of a 3×3 partitioned block matrix, we have successfully accomplished the algorithmic formulation of the solution for $\mathbf{x}_h(k)$, $\mathbf{w}_h(k)$ and $\mathbf{k}_h(k)$ inclusive of some further relevant contents, e.g., the residual vectors and redundancy contribution and redundant indexes of the measurements etc.

Before the solution is delivered, the equivalency of (3.36) to (3.8) and (3.23) is first proved. With the 2^{nd} equation in (3.36), three specifics need readers' attention for the benefit of further derivation:

i) The coefficient matrix of $\boldsymbol{x}_h(k)$ in the 1st equation of (3.26) is $\boldsymbol{D}_{xx}^{-1}(k/k)$ (refer to (3.24)).

ii) The inverse of the coefficient matrix of $w_h(k)$ in the 2nd equation of (3.26) gives

$$[\mathbf{B}^{T}(k)\mathbf{D}_{l_{x}l_{x}}^{-1}(k)\mathbf{B}(k) + \mathbf{Q}^{-1}(k)]^{-1}$$

= $\mathbf{Q}(k) - \mathbf{Q}(k)\mathbf{B}^{T}(k)\mathbf{D}_{xx}^{-1}(k/k-1)\mathbf{B}(k)\mathbf{Q}(k)$ (3.37)

iii) Solving for $w_h(k)$ from the 2nd equation in (3.26) gives

$$\boldsymbol{w}_{h}(k) = [\boldsymbol{Q}(k) - \boldsymbol{Q}(k)\boldsymbol{B}^{T}(k)\boldsymbol{D}_{xx}^{-1}(k/k-1)\boldsymbol{B}(k)\boldsymbol{Q}(k)] \cdot \boldsymbol{B}^{T}(k)\boldsymbol{D}_{l_{x}l_{x}}^{-1}(k)\boldsymbol{x}_{h}(k) + [\boldsymbol{Q}(k) - \boldsymbol{Q}(k)\boldsymbol{B}^{T}(k)\boldsymbol{D}_{xx}^{-1}(k/k-1)\boldsymbol{B}(k)\boldsymbol{Q}(k)] \cdot (3.38) \cdot [-\boldsymbol{B}^{T}(k)\boldsymbol{D}_{l_{x}l_{x}}^{-1}(k)\boldsymbol{l}_{x}(k) + \boldsymbol{Q}^{-1}(k)\boldsymbol{l}_{w}(k)]$$

Substituting (3.38) into the 1st equation of (3.36) eliminates $w_h(k)$

$$\begin{pmatrix} \boldsymbol{D}_{xx}^{-1}(k/k) & \boldsymbol{H}(k) \\ \boldsymbol{H}^{T}(k) & \boldsymbol{O} \end{pmatrix} \begin{pmatrix} \boldsymbol{x}_{h}(k) \\ \boldsymbol{k}_{h}(k) \end{pmatrix} = \\ \begin{pmatrix} \boldsymbol{D}_{xx}^{-1}(k/k-1)\boldsymbol{x}(k/k-1) + \boldsymbol{C}^{T}(k)\boldsymbol{R}^{-1}(k)\boldsymbol{z}(k) \\ \boldsymbol{h} \end{pmatrix}$$
(3.39)

which proved that (3.36) is equivalent to (3.8) and (3.23) for $\mathbf{x}_{h}(k)$ and $\mathbf{k}_{h}(k)$ as

$$D_{xx}^{-1}(k/k-1)[I_{x}(k) + B(k)I_{w}(k)] + C^{T}(k)R^{-1}(k)z(k)$$

= $D_{xx}^{-1}(k/k-1)x(k/k-1) + C^{T}(k)R^{-1}(k)z(k)$
= $D_{xx}^{-1}(k)x(k)$ (3.40)

3.5 Solution

Now, without providing the lengthy intermediate steps, the solution of $\boldsymbol{x}_h(k)$, $\boldsymbol{w}_h(k)$ and $\boldsymbol{k}_h(k)$ is directly given below:

$$\boldsymbol{x}_{h}(k) = \boldsymbol{x}(k/k-1) + \boldsymbol{K}(k)\boldsymbol{d}(k) - \boldsymbol{D}_{xx}(k/k)\boldsymbol{H}(k)\boldsymbol{k}_{h}(k)$$
(3.41)

$$\boldsymbol{w}_{h}(k) = \boldsymbol{l}_{w}(k) + \boldsymbol{Q}(k)\boldsymbol{B}^{T}(k)\boldsymbol{D}_{xx}^{-1}(k/k-1)\boldsymbol{K}(k)\boldsymbol{d}(k) -\boldsymbol{Q}(k)\boldsymbol{B}^{T}(k)\boldsymbol{D}_{xx}^{-1}(k/k-1)\boldsymbol{D}_{xx}(k/k) \cdot \cdot\boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)[\boldsymbol{H}^{T}(k)\boldsymbol{x}(k/k)-\boldsymbol{h}]$$
(3.42)

$$\boldsymbol{k}_{h}(k) = \boldsymbol{N}_{hh}^{-1}(k) \{ \boldsymbol{H}^{T}(k) \boldsymbol{D}_{xx}(k/k) \cdot [\boldsymbol{D}_{l_{x}l_{x}}^{-1}(k)\boldsymbol{x}(k/k-1) + \boldsymbol{C}^{T}(k)\boldsymbol{R}^{-1}(k)\boldsymbol{z}(k)] - \boldsymbol{h} \}$$
(3.43)

with the variance–covariance matrices of $\boldsymbol{x}_h(k)$ and $\boldsymbol{w}_h(k)$:

$$\boldsymbol{D}_{x_h x_h}(k) = \boldsymbol{D}_{xx}(k/k-1)$$

-
$$\boldsymbol{D}_{xx}(k/k-1)\boldsymbol{C}^{T}(k)\boldsymbol{D}_{dd}^{-1}(k)\boldsymbol{C}(k)\boldsymbol{D}_{xx}(k/k-1)$$
 (3.44)
-
$$\boldsymbol{D}_{xx}(k/k)\boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)\boldsymbol{H}^{T}(k)\boldsymbol{D}_{xx}(k/k)$$

$$D_{w_h w_h}(k) = Q(k)$$

$$-Q(k)B^{T}(k)C^{T}(k)D_{dd}^{-1}(k)C(k)B(k)Q(k) \qquad (3.45)$$

$$-Q(k)B^{T}(k)[I - K(k)C(k)]^{T} \cdot \cdot H(k)N_{hh}^{-1}(k)H^{T}(k)[I - K(k)C(k)]B(k)Q(k)$$

$$D_{x_h w_h}(k-1) = [I - D_{xx}(k/k)H(k)N_{hh}^{-1}(k)H^{T}(k)] \cdot \cdot [I - K(k)C(k)]B(k)Q(k) \qquad (3.46)$$

3.6 Solutions with and without Constraints

The solution of $\mathbf{x}_h(k)$ and $\mathbf{w}_h(k)$ in discrete Kalman filtering with constraints is connected to the solution of $\mathbf{x}(k)$ and $\mathbf{w}(k)$ (without constraints) given in Section 2.3 as follows:

$$\boldsymbol{x}_{h}(k) = \boldsymbol{x}(k/k)$$

$$-\boldsymbol{D}_{xx}(k/k)\boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)[\boldsymbol{H}^{T}(k)\boldsymbol{x}(k/k) - \boldsymbol{h}]$$

$$\boldsymbol{w}_{h}(k) = \boldsymbol{w}(k) - \boldsymbol{Q}(k)\boldsymbol{B}^{T}(k)\boldsymbol{D}_{xx}^{-1}(k/k - 1)\boldsymbol{D}_{xx}(k/k) \cdot \cdot \boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)[\boldsymbol{H}^{T}(k)\boldsymbol{x}(k/k) - \boldsymbol{h}]$$
(3.47)
$$(3.47)$$

$$D_{x_h x_h}(k) = D_{xx}(k/k)$$

$$-D_{xx}(k/k)H(k)N_{hh}^{-1}(k)H^{T}(k)D_{xx}(k/k)$$

$$D_{w_h w_h}(k-1) = D_{ww}(k)$$

$$-Q(k)B^{T}(k)D_{xx}^{-1}(k/k-1)D_{xx}(k/k)H(k)N_{hh}^{-1}(k)$$

$$\cdot H^{T}(k)D_{xx}(k/k)D_{xx}^{-1}(k/k-1)B(k)Q(k)$$
(3.50)

$$\boldsymbol{D}_{x_h \boldsymbol{w}_h}(k-1) = \boldsymbol{D}_{xw}(k) - \boldsymbol{D}_{xx}(k/k)\boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k) \cdot \boldsymbol{H}^T(k)[\boldsymbol{I} - \boldsymbol{K}(k)\boldsymbol{C}(k)]\boldsymbol{B}(k)\boldsymbol{Q}(k) (3.51)$$

This group of formulas provides the opportunity to obtain the solution with constraints directly upon the solution from the standard Kalman filtering described in Section 2. A hard-won advantage of the solution expressions from (3.47) to (3.51) lies in first obtaining the solution after (2.3) (or (2.18)), (2.19), (2.4), (2.20) and (2.21) without considering the constraints and then utilizing $\mathbf{x}(k/k)$ to linearize the constraints, when they are nonlinear, and apply them towards the solution with constraints.

3.7 Residual Vectors and their Variance Matrices

For error analysis in Kalman filtering, $v_{x_k}(k)$,

 $\mathbf{v}_{w_h}(k)$ (when $\mathbf{w}_0(k) = \mathbf{o}$) and $\mathbf{v}_{z_h}(k)$ with their associated covariance matrices are further derived below.

In general, they can directly be calculated according to (3.32) or individually after (3.25), (3.28) and (3.17). However, they are further detailed.

<u>First</u>, with the residual vector $v_x^h(k)$ of $l_x(k)$ in (3.25), substituting (3.41) and (3.42) or (3.47) and (3.48) into (3.25) gives

$$\mathbf{v}_{l_x}^{h}(k) = \mathbf{x}(k/k) - \mathbf{l}_x(k) - \mathbf{B}(k)\mathbf{w}(k)$$

- $\mathbf{D}_{xx}(k/k)\mathbf{H}(k)\mathbf{N}_{hh}^{-1}(k)[\mathbf{H}^{T}(k)\mathbf{x}(k/k) - \mathbf{h}] (3.52)$
+ $\mathbf{B}(k)\mathbf{Q}(k)\mathbf{B}^{T}(k)\mathbf{D}_{xx}^{-1}(k/k - 1)\mathbf{D}_{xx}(k/k) \cdot$
 $\cdot \mathbf{H}(k)\mathbf{N}_{hh}^{-1}(k)[\mathbf{H}^{T}(k)\mathbf{x}(k/k) - \mathbf{h}]$

or

$$\boldsymbol{v}_{l_x}^{h}(k) = \boldsymbol{D}_{l_x l_x}(k) \boldsymbol{D}_{xx}^{-1}(k/k-1)\boldsymbol{K}(k)\boldsymbol{d}(k)$$

$$-\boldsymbol{D}_{l_x l_x}(k) [\boldsymbol{I} - \boldsymbol{K}(k)\boldsymbol{C}(k)]^{T} \cdot (3.52a)$$

$$\cdot \boldsymbol{H}(k) \boldsymbol{N}_{hh}^{-1}(k) [\boldsymbol{H}^{T}(k)\boldsymbol{x}(k/k) - \boldsymbol{h}]$$

Based on (2.22), (3.52) is further simplified to

$$\mathbf{v}_{l_x}^h(k) = \mathbf{v}_{l_x}(k) - [\mathbf{I} + \mathbf{B}(k)\mathbf{Q}(k)\mathbf{B}^T(k)\mathbf{D}_{xx}^{-1}(k/k-1)]$$

 $\cdot \mathbf{D}_{xx}(k/k)\mathbf{H}(k)\mathbf{N}_{hh}^{-1}(k)[\mathbf{H}^T(k)\mathbf{x}(k/k) - \mathbf{h}]$ (3.53)

<u>Second</u>, with the residual vector $\mathbf{v}_{w_h}(k)$ of $\mathbf{l}_w(k)$ in (3.28), the substitution of (3.42) or (3.48) yields

$$\boldsymbol{v}_{w}^{h}(k) = \boldsymbol{w}(k) - \boldsymbol{Q}(k)\boldsymbol{B}^{T}(k)\boldsymbol{D}_{xx}^{-1}(k/k-1)\boldsymbol{D}_{xx}(k/k)$$
$$\cdot \boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)[\boldsymbol{H}^{T}(k)\boldsymbol{x}(k/k) - \boldsymbol{h}] - \boldsymbol{l}_{w}(k) \quad (3.54)$$

or

$$\boldsymbol{v}_{l_{w}}^{h}(k) = \boldsymbol{Q}(k)\boldsymbol{B}^{T}(k)\boldsymbol{D}_{xx}^{-1}(k/k-1)\boldsymbol{K}(k)\boldsymbol{d}(k) -\boldsymbol{Q}(k)\boldsymbol{B}^{T}(k)[\boldsymbol{I}-\boldsymbol{K}(k)\boldsymbol{C}(k)]^{T} \cdot\boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)[\boldsymbol{H}^{T}(k)\boldsymbol{x}(k/k)-\boldsymbol{h}]$$
(3.54a)

After (2.23), (3.54) is further reformed to

$$\boldsymbol{v}_{l_w}^h(k) = \boldsymbol{v}_{l_w}(k) - \boldsymbol{Q}(k)\boldsymbol{B}^T(k)\boldsymbol{D}_{xx}^{-1}(k/k-1)\boldsymbol{D}_{xx}(k/k)$$
$$\cdot \boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)[\boldsymbol{H}^T(k)\boldsymbol{x}(k/k) - \boldsymbol{h}] \quad (3.55)$$

Because the initial value of $l_w(k)$ is usually assumed to be: $w_0(k) = o$ in practice, (3.54) becomes

$$\boldsymbol{v}_{l_w}^h(k) = \boldsymbol{w}(k) - \boldsymbol{Q}(k)\boldsymbol{B}^T(k)\boldsymbol{D}_{xx}^{-1}(k/k-1)\boldsymbol{D}_{xx}(k/k)$$
$$\cdot \boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)[\boldsymbol{H}^T(k)\boldsymbol{x}(k/k) - \boldsymbol{h}] \quad (3.56)$$

<u>*Third*</u>, with the residual vector $\mathbf{v}_{z}^{h}(k)$ of $\mathbf{l}_{z}(k) = z(k)$, substituting (3.41) or (3.47) into (3.17) delivers:

$$\boldsymbol{v}_{z}^{h}(k) = \boldsymbol{C}(k) \{ \boldsymbol{x}(k/k) - \boldsymbol{D}_{xx}(k/k)\boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)$$

$$\cdot [\boldsymbol{H}^{T}(k)\boldsymbol{x}(k/k) - \boldsymbol{h}] \} - \boldsymbol{l}_{z}(k)$$
(3.57)

or

$$\boldsymbol{v}_{z}^{h}(k) = [\boldsymbol{C}(k)\boldsymbol{K}(k) - \boldsymbol{I}]\boldsymbol{d}(k) - \boldsymbol{C}(k)\boldsymbol{D}_{xx}(k/k)$$
$$\cdot \boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)[\boldsymbol{H}^{T}(k)\boldsymbol{x}(k/k) - \boldsymbol{h}] \quad (3.58)$$

According to (2.24), (3.58) is simplified to

$$\boldsymbol{v}_{z}^{h}(k) = \boldsymbol{v}_{z}(k) - \boldsymbol{C}(k)\boldsymbol{D}_{xx}(k/k)$$

$$\cdot \boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)[\boldsymbol{H}^{T}(k)\boldsymbol{x}(k/k) - \boldsymbol{h}]$$
(3.59)

The covariance matrix of the residual vectors for each of $\mathbf{v}_{x_h}(k)$, $\mathbf{v}_{w_h}(k)$ and $\mathbf{v}_{z_h}(k)$ are derived as follows:

(1) $D_{v_{l_x}^{h,v_{l_x}^{h}}}(k)$ is derived by applying the law of variance propagation to (3.52a)

$$\boldsymbol{D}_{\boldsymbol{v}_{x}^{h}\boldsymbol{v}_{x}^{h}}(k) = \boldsymbol{D}_{l_{x}l_{x}}(k)\boldsymbol{C}^{T}(k)\boldsymbol{D}_{dd}^{-1}(k)\boldsymbol{C}(k)\boldsymbol{D}_{l_{x}l_{x}}(k)$$
$$+ \boldsymbol{D}_{l_{x}l_{x}}(k)[\boldsymbol{I} - \boldsymbol{K}(k)\boldsymbol{C}(k)]^{T}\boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)$$
$$\cdot \boldsymbol{H}^{T}(k)[\boldsymbol{I} - \boldsymbol{K}(k)\boldsymbol{C}(k)]\boldsymbol{D}_{l_{x}l_{x}}(k) \qquad (3.60)$$

as $D_{xd}(k) = 0$ in (2.10). Under the consideration of (2.25), (3.60) becomes

$$\boldsymbol{D}_{\boldsymbol{\nu}_{x}^{h}\boldsymbol{\nu}_{x}^{h}}(k) = \boldsymbol{D}_{\boldsymbol{\nu}_{x}\boldsymbol{\nu}_{x}}(k) + \boldsymbol{D}_{l,l_{x}}(k)\boldsymbol{D}_{xx}^{-1}(k/k-1)\boldsymbol{D}_{xx}(k/k)$$

$$\cdot\boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)\boldsymbol{H}^{T}(k)\boldsymbol{D}_{xx}(k/k)\boldsymbol{D}_{xx}^{-1}(k/k-1)\boldsymbol{D}_{l_{x}l_{x}}(k)$$

(3.61)

(2) $D_{v_{l_w}^h v_{l_w}^h}(k)$ is developed similarly by applying the law of variance propagation to (3.54a) :

$$D_{\nu_{w}^{h}\nu_{w}^{h}}(k) = Q(k)B^{T}(k)C^{T}(k)D_{dd}^{-1}(k)C(k)B(k)Q(k)$$

+ Q(k)B^{T}(k)[I - K(k)C(k)]^{T}H(k)N_{hh}^{-1}(k)
· H^T(k)[I - K(k)C(k)]B(k)Q(k) (3.62)

and further, based on (2.26),

$$D_{\boldsymbol{\nu}_{w}^{h}\boldsymbol{\nu}_{w}^{h}}(k) = D_{\boldsymbol{\nu}_{w}\boldsymbol{\nu}_{w}}(k)$$

+ $Q(k)B^{T}(k)D_{xx}^{-1}(k/k-1)D_{xx}(k/k)H(k)N_{hh}^{-1}(k)$
 $\cdot H^{T}(k)D_{yy}(k/k)D_{yy}^{-1}(k/k-1)B(k)Q(k)$ (3.63)

(3) $D_{\nu_{z}^{h}\nu_{z}^{h}}(k)$ is given by applying the law of variance propagation to (3.58)

$$\boldsymbol{D}_{\boldsymbol{p}_{z}^{h}\boldsymbol{p}_{z}^{h}}(k) = [\boldsymbol{I} - \boldsymbol{C}(k)\boldsymbol{K}(k)]\boldsymbol{R}(k) + \boldsymbol{C}(k)\boldsymbol{D}_{xx}(k/k)$$
$$\cdot \boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)\boldsymbol{H}^{T}(k)\boldsymbol{D}_{xx}(k/k)\boldsymbol{C}^{T}(k) \quad (3.64)$$

and further according to (2.24),

$$D_{\boldsymbol{v}_{z}^{h}\boldsymbol{v}_{z}^{h}}(k) = D_{\boldsymbol{v}_{z}\boldsymbol{v}_{z}}(k) + C(k)D_{xx}(k/k)$$

$$\cdot \boldsymbol{H}(k)N_{hh}^{-1}(k)\boldsymbol{H}^{T}(k)D_{xx}(k/k)\boldsymbol{C}^{T}(k)$$
(3.65)

3.8 Redundancy Contribution of Measurements

There are two levels of redundancy contribution: the total redundancy contribution of $l_x(k)$, $l_w(k)$ and z(k) together as well as the subtotal redundancy contribution of each of the groups, and the individual redundant indexes associated with each element in a group of the independent measurements, here specifically $l_w(k)$ and z(k) because Q(k) and R(k) are commonly diagonal in practice. The following discusses the redundancy contributions of $l_x(k)$, $l_w(k)$ and $l_z(k)$ one by one:

(1) The redundancy contribution $r_{l_x}(k)$ of $l_x(k)$

$$r_{l_{x}}(k) = tr\{D_{v_{x}^{h}v_{x}^{h}}(k)D_{l_{x}l_{x}}^{-1}(k)\}$$

= $tr\{D_{l_{x}l_{x}}(k)C^{T}(k)D_{dd}^{-1}(k)C(k)\}$
+ $tr\{D_{l_{x}l_{x}}(k)D_{xx}^{-1}(k/k-1)D_{xx}(k/k)H(k)N_{hh}^{-1}(k)$
 $\cdot H^{T}(k)D_{xx}(k/k)D_{xx}^{-1}(k/k-1)\}$ (3.66)

However, no individual redundant indexes will have the usual meaning for $l_x(k)$ as its variance matrix of $D_{l_x l_x}(k) =$ $A(k,k-1)D_{xx}(k-1)A^T(k,k-1)$ will not be possibly diagonal in reality.

(2) The redundancy contribution $r_{l_w}(k)$ of $l_w(k)$

$$r_{l_{w}}(k) = tr\{D_{v_{w}^{h}v_{w}^{h}}(k)D_{l_{w}l_{w}}^{-1}(k)\}$$

= $tr\{D_{v_{w}v_{w}}(k)Q^{-1}(k)\}$
+ $tr\{Q(k)B^{T}(k)D_{xx}^{-1}(k/k-1)D_{xx}(k/k)H(k)N_{hh}^{-1}(k)$
 $\cdot H^{T}(k)D_{xx}(k/k)D_{xx}^{-1}(k/k-1)B(k)\}$ (3.67)
or

$$r_{l_w}(k) = tr\{\boldsymbol{Q}(k)\boldsymbol{B}^{T}(k)\boldsymbol{C}^{T}(k)\boldsymbol{D}_{dd}^{-1}(k)\boldsymbol{C}(k)\boldsymbol{B}(k)\}$$

+ $tr\{\boldsymbol{Q}(k)\boldsymbol{B}^{T}(k)\boldsymbol{D}_{xx}^{-1}(k/k-1)\boldsymbol{D}_{xx}(k/k)\boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)$
 $\cdot \boldsymbol{H}^{T}(k)\boldsymbol{D}_{xx}(k/k)\boldsymbol{D}_{xx}^{-1}(k/k-1)\boldsymbol{B}(k)\}$ (3.68)

Besides, the individual redundant index associated with each component in $l_w(k)$, when Q(k) is diagonal, is derived as follows

$$r_{l_{w}}^{i}(k) = \{Q(k)B^{T}(k)C^{T}(k)D_{dd}^{-1}(k)C(k)B(k)\}_{ii} + \{Q(k)B^{T}(k)D_{xx}^{-1}(k/k-1)D_{xx}(k/k)H(k)N_{hh}^{-1}(k) \cdot H^{T}(k)D_{xx}(k/k)D_{xx}^{-1}(k/k-1)B(k)\}_{ii} (i = 1, 2, ..., m)$$
(3.69)

(3) The redundancy contribution $r_{l_z}(k)$ (or $r_z(k)$) for $l_z(k)$ (or z(k))

$$r_{z}(k) = trace\{\boldsymbol{D}_{\boldsymbol{v}_{z}^{h}\boldsymbol{v}_{z}^{h}}(k)\boldsymbol{D}_{l_{z}l_{z}}^{-1}(k)\}$$

$$= tr\{\boldsymbol{D}_{\boldsymbol{v}_{z}\boldsymbol{v}_{z}}(k)\boldsymbol{R}^{-1}(k)\}$$

$$+ tr\{\boldsymbol{C}(k)\boldsymbol{D}_{xx}(k/k)\boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)$$

$$\cdot\boldsymbol{H}^{T}(k)\boldsymbol{D}_{xx}(k/k)\boldsymbol{C}^{T}(k)\boldsymbol{R}^{-1}(k)\}$$

(3.70)

in which the first item is

$$tr\{\boldsymbol{D}_{\boldsymbol{y},\boldsymbol{y}_{z}}(k)\boldsymbol{R}^{-1}(k)\} = tr\{[\boldsymbol{I} - \boldsymbol{C}(k)\boldsymbol{K}(k)]\boldsymbol{R}(k)\boldsymbol{R}^{-1}(k)\}$$
$$= tr[\boldsymbol{I}_{p \times p} - \boldsymbol{C}(k)\boldsymbol{K}(k)]$$
$$= p(k) - tr[\boldsymbol{C}(k)\boldsymbol{K}(k)]$$
(3.71)

When $\mathbf{R}(k)$ is diagonal, the individual redundant index with each component in $l_{z}(k)$ is

$$r_{z}^{i}(k) = \{ \boldsymbol{D}_{\boldsymbol{v}_{z}\boldsymbol{v}_{z}}(k)\boldsymbol{R}^{-1}(k) \}_{ii} + \{ \boldsymbol{C}(k)\boldsymbol{D}_{xx}(k/k)\boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k) \\ \cdot \boldsymbol{H}^{T}(k)\boldsymbol{D}_{xx}(k/k)\boldsymbol{C}^{T}(k)\boldsymbol{R}^{-1}(k) \}_{ii}$$
(3.72)

and further

$$\mathbf{r}_{z}^{l}(k) = [\mathbf{I} - \mathbf{C}(k)\mathbf{K}(k)]_{ii} + [\mathbf{C}(k)\mathbf{D}_{xx}(k/k)\mathbf{H}(k)\mathbf{N}_{hh}^{-1}(k)]$$
$$\cdot \mathbf{H}^{T}(k)\mathbf{D}_{xx}(k/k)\mathbf{C}^{T}(k)\mathbf{R}^{-1}(k)]_{ii}$$
$$(i = 1, 2, ..., p) \qquad (3.73)$$

Finally, the total redundancy contribution of the three independent observation vectors together at epoch k, i.e., total redundancy number of $l_x(k)$,

 $l_w(k)$ and $l_z(k)$ together is equal to

$$r(k) = r_{l_x}(k) + r_{l_w}(k) + r_z(k)$$
(3.74)

with the following specific detail,

$$r(k) = tr\{D_{l_{x}l_{x}}(k)C^{T}(k)D_{dd}^{-1}(k)C(k)\}$$

$$+ tr\{D_{l_{x}l_{x}}(k)D_{xx}^{-1}(k/k-1)D_{xx}(k/k)H(k)N_{hh}^{-1}(k)$$

$$\cdot H^{T}(k)D_{xx}(k/k)D_{xx}^{-1}(k/k-1)\}$$

$$+ tr\{Q(k)B^{T}(k)C^{T}(k)D_{dd}^{-1}(k)C(k)B(k)\}$$

$$+ tr\{Q(k)B^{T}(k)D_{xx}^{-1}(k/k-1)D_{xx}(k/k)H(k)$$

$$\cdot N_{hh}^{-1}(k)H^{T}(k)D_{xx}(k/k)D_{xx}^{-1}(k/k-1)B(k)\}$$

$$+ tr\{I - C(k)K(k)\}$$

$$+ tr\{C(k)D_{xx}(k/k)H(k)N_{hh}^{-1}(k)H^{T}(k)D_{xx}(k/k)$$

$$\cdot C^{T}(k)R^{-1}(k)\}$$

It can be proved that the total redundant index at epoch k is equal to

$$r(k) = p(k) + tr\{N_{hh}^{-1}(k)H^{T}(k)D_{xx}(k/k)H(k)\}$$

= $p(k) + tr\{I_{hxh}\} = p(k) + h(k)$ (3.75)

which means

$$r(k) = r_{l_x}(k) + r_{l_w}(k) + r_z(k) = p(k) + h(k) \quad (3.76)$$

with p(k) and h(k) being the number of the measurements in z(k) and the number of the constraints in (3.1).

3.9 Other Aspects

In addition, several algorithmic developments such as test statistics, variance factors and variance component estimation etc. may be further conducted, in analogy to the work in [Wang, 1997, 2008, 2009 etc.] and are excluded here due to the space restriction, except the following essential remark about the variance of unit weight:

- (i) The variance of unit weight for Section 2 (standard discrete Kalman filter): the one in (2.34) is identical to the one in (2.35).
- (ii) The variance of unit weight for Section 3 (discrete Kalman filter with constraints):

$$\hat{\sigma}_{0}^{2} = [\boldsymbol{v}_{l_{x}}^{hT}(k)\boldsymbol{D}_{l_{x}l_{x}}^{-1}(k)\boldsymbol{v}_{l_{x}}^{h}(k) + \boldsymbol{v}_{l_{w}}^{hT}(k)\boldsymbol{Q}^{-1}(k)\boldsymbol{v}_{l_{w}}^{h}(k) + \boldsymbol{v}_{z}^{hT}(k)\boldsymbol{R}^{-1}(k)\boldsymbol{v}_{z}^{h}(k)]/r(k)$$
(3.77)

as

$$d^{T}(k)D_{dd}^{-1}(k)d(k) \neq [\mathbf{v}_{l_{x}}^{hT}(k)D_{l_{x}l_{x}}^{-1}(k)\mathbf{v}_{l_{x}}^{h}(k) + \mathbf{v}_{l_{w}}^{hT}(k)\mathbf{Q}^{-1}(k)\mathbf{v}_{l_{w}}^{h}(k) + \mathbf{v}_{z}^{hT}(k)\mathbf{R}^{-1}(k)\mathbf{v}_{z}^{h}(k)]$$
(3.78)

4. Algorithm in the Form of Extended Kalman Filter with Constraints

This section frames the relevant formulas in the form of Extended Kalman filter in accordance with the functional model defined in Section 3.1, but having them (i.e., (2.1), (2.2) and (3.1)) nonlinear.

The system model, the measurement model and constraint model appear nonlinear as follows:

$$\mathbf{x}(k) = \mathbf{A}(\mathbf{x}(k-1), k) + \mathbf{B}(k, k-1)\mathbf{w}(k-1)$$
(4.1)

$$z(k) = C(x(k), k) + \Delta(k)$$
(4.2)

$$\boldsymbol{H}(\boldsymbol{x}(k),k) - \boldsymbol{h} = \boldsymbol{o} \tag{4.3}$$

As for the variance propagation, three Jacobian matrices are derived here,

$$A(k,k-1) = A(k) = \frac{\partial A(x(k-1),k)}{\partial x_{1}(k-1)} = \begin{pmatrix} \frac{\partial A_{1}(x(k-1),k)}{\partial x_{1}(k-1)} & \frac{\partial A_{1}(x(k-1),k)}{\partial x_{2}(k-1)} & \cdots & \frac{\partial A_{1}(x(k-1),k)}{\partial x_{n}(k-1)} \\ \frac{\partial A_{2}(x(k-1),k)}{\partial x_{1}(k-1)} & \frac{\partial A_{2}(x(k-1),k)}{\partial x_{2}(k-1)} & \cdots & \frac{\partial A_{2}(x(k-1),k)}{\partial x_{n}(k-1)} \\ \vdots & \vdots & \ddots & \vdots \\ \frac{\partial A_{n}(x(k-1),k)}{\partial x_{1}(k-1)} & \frac{\partial A_{n}(x(k-1),k)}{\partial x_{2}(k-1)} & \cdots & \frac{\partial A_{n}(x(k-1),k)}{\partial x_{n}(k-1)} \\ \end{pmatrix}$$
(4.4)

which is with respect to the estimated state vector $\mathbf{x}(k-1/k-1)$ at t_{k-1} ,

$$C(k) = \frac{\partial C(\mathbf{x}(k), k)}{\partial \mathbf{x}_{1}(k)} = \begin{pmatrix} \frac{\partial C_{1}(\mathbf{x}(k), k)}{\partial \mathbf{x}_{1}(k)} & \frac{\partial C_{1}(\mathbf{x}(k), k)}{\partial \mathbf{x}_{2}(k)} & \cdots & \frac{\partial C_{1}(\mathbf{x}(k), k)}{\partial \mathbf{x}_{n}(k)} \\ \frac{\partial C_{2}(\mathbf{x}(k), k)}{\partial \mathbf{x}_{1}(k)} & \frac{\partial C_{2}(\mathbf{x}(k), k)}{\partial \mathbf{x}_{2}(k)} & \cdots & \frac{\partial C_{2}(\mathbf{x}(k), k)}{\partial \mathbf{x}_{n}(k)} \\ \vdots & \vdots & \vdots & \vdots \\ \frac{\partial C_{p}(\mathbf{x}(k), k)}{\partial \mathbf{x}_{1}(k)} & \frac{\partial C_{p}(\mathbf{x}(k), k)}{\partial \mathbf{x}_{2}(k)} & \cdots & \frac{\partial C_{p}(\mathbf{x}(k), k)}{\partial \mathbf{x}_{n}(k)} \end{pmatrix}$$
(4.5)

which is with respect to the predicted state vector $\mathbf{x}(k/k-1)$ through the time update from t_{k-1} to t_k , and

$$\boldsymbol{H}^{T}(k) = \frac{\partial \boldsymbol{H}(\boldsymbol{x}(k),k)}{\partial \boldsymbol{x}_{1}(k)} = \begin{pmatrix} \frac{\partial \boldsymbol{H}_{1}(\boldsymbol{x}(k),k)}{\partial \boldsymbol{x}_{1}(k)} & \frac{\partial \boldsymbol{H}_{1}(\boldsymbol{x}(k),k)}{\partial \boldsymbol{x}_{2}(k)} & \cdots & \frac{\partial \boldsymbol{H}_{1}(\boldsymbol{x}(k),k)}{\partial \boldsymbol{x}_{n}(k)} \\ \frac{\partial \boldsymbol{H}_{2}(\boldsymbol{x}(k),k)}{\partial \boldsymbol{x}_{1}(k)} & \frac{\partial \boldsymbol{H}_{2}(\boldsymbol{x}(k),k)}{\partial \boldsymbol{x}_{2}(k)} & \cdots & \frac{\partial \boldsymbol{H}_{2}(\boldsymbol{x}(k),k)}{\partial \boldsymbol{x}_{n}(k)} \\ \vdots & \vdots & \vdots \\ \frac{\partial \boldsymbol{H}_{h}(\boldsymbol{x}(k),k)}{\partial \boldsymbol{x}_{1}(k)} & \frac{\partial \boldsymbol{H}_{h}(\boldsymbol{x}(k),k)}{\partial \boldsymbol{x}_{2}(k)} & \cdots & \frac{\partial \boldsymbol{H}_{h}(\boldsymbol{x}(k),k)}{\partial \boldsymbol{x}_{n}(k)} \end{pmatrix} \end{pmatrix}$$
(4.6)

which is with respect to the estimated state vector $\mathbf{x}(k)$ through the measurement update before the constraints are applied at t_k .

The following gives the algorithm in the form of

Extended Kalman filter by referring to Sections 3.4 and 3.5:

1) THE MEASUREMENT MODEL

The predicted state vector exclusive of the effect from the process noise vector:

$$\mathbf{v}_{x}(k) = \mathbf{x}_{h}(k) - \mathbf{B}(k, k-1)\mathbf{w}_{h}(k-1) - \mathbf{l}_{x}(k) \qquad (3.25)$$

$$l_x(k) = A(x_h(k-1), k, k-1)$$
 (vs. (3.26)) (4.7)

$$\boldsymbol{D}_{l_{x}l_{x}}(k) = \boldsymbol{A}(k,k-1)\boldsymbol{D}_{xx}(k-1)\boldsymbol{A}^{T}(k,k-1) \qquad (3.27)$$

The process noise vector as a group of the pseudomeasurements: the same as (3.28), (3.29) and (3.30).

A group of the measurements from the measurement vector z(k) at t_k :

$$v_{l_z}(k) = C(x_h(k), k) - l_z(k)$$
 (vs. (3.17)) (4.8)

 $l_{z}(k) = z(k) \tag{3.18}$

$$\boldsymbol{D}_{l,l_{\star}}(k) = \boldsymbol{R}(k) \tag{3.19}$$

A group of the constraints on the states:

$$H(x_h(k),k) - h = o$$
 (vs. (3.1)) (4.9)

2) THE SOLUTION

The state vector, the process noise vector and the Lagrange multiplier vector:

$$\boldsymbol{x}_{h}(k/k) = \boldsymbol{x}(k/k) - \boldsymbol{D}_{xx}(k/k)\boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)[\boldsymbol{H}(\boldsymbol{x}(k/k),k) - \boldsymbol{h}]$$
(4.10)

$$w_{h}(k-1) = I_{w}(k)$$

+ $Q(k)B^{T}(k)D_{xx}^{-1}(k/k-1)K(k)d(k)$
- $Q(k)B^{T}(k)D_{xx}^{-1}(k/k-1)D_{xx}(k/k)$ (4.11)

$$\cdot \boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)[\boldsymbol{H}(\boldsymbol{x}(k/k),k)-\boldsymbol{h}]$$

$$\boldsymbol{k}_{h}(k) = \boldsymbol{N}_{hh}^{-1}(k) [\boldsymbol{H}(\boldsymbol{x}(k/k), k) - \boldsymbol{h}]$$
(4.12)
wherein

$$\boldsymbol{x}(k/k) = \boldsymbol{x}(k/k-1) + \boldsymbol{K}(k)\boldsymbol{d}(k)$$
(4.13)

$$\mathbf{x}(k/k-1) = \mathbf{A}(\mathbf{x}_{h}(k-1), k, k-1) + \mathbf{B}(k)\mathbf{w}_{0}(k) \quad (4.14)$$

$$d(k) = z(k) - A(x_h(k-1), k, k-1) - B(k)w_0(k)$$
(4.15)

The var-covariance matrices of the state vector and the process noise vector: the same as (3.49), (3.50) and (3.51).

3) THE MEASUREMENT RESIDUALS

The residual vectors:

$$\boldsymbol{v}_{l_{x}}^{h}(k) = \boldsymbol{D}_{l_{x}l_{x}}(k)\boldsymbol{D}_{xx}^{-1}(k/k-1)\boldsymbol{K}(k)\boldsymbol{d}(k)$$

$$-\boldsymbol{D}_{l_{x}l_{x}}(k)[\boldsymbol{I}-\boldsymbol{K}(k)\boldsymbol{C}(k)]^{T} \qquad (4.16)$$

$$\cdot\boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)[\boldsymbol{H}(\boldsymbol{x}(k/k),k)-\boldsymbol{h}]$$

$$\boldsymbol{v}_{l_{w}}^{h}(k) = \boldsymbol{Q}(k)\boldsymbol{B}^{T}(k)\boldsymbol{D}_{xx}^{-1}(k/k-1)\boldsymbol{K}(k)\boldsymbol{d}(k)$$

$$-\boldsymbol{Q}(k)\boldsymbol{B}^{T}(k)[\boldsymbol{I}-\boldsymbol{K}(k)\boldsymbol{C}(k)]^{T} \qquad (4.17)$$

$$\cdot\boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)[\boldsymbol{H}(\boldsymbol{x}(k/k),k)-\boldsymbol{h}]$$

$$\boldsymbol{v}_{z}^{h}(k) = [\boldsymbol{C}(k)\boldsymbol{K}(k) - \boldsymbol{I}]\boldsymbol{d}(k) - \boldsymbol{C}(k)\boldsymbol{D}_{xx}(k/k)$$

$$\cdot \boldsymbol{H}(k)\boldsymbol{N}_{hh}^{-1}(k)[\boldsymbol{H}(\boldsymbol{x}(k/k),k) - \boldsymbol{h}]$$
(4.18)

The variance matrices of the residual vectors: are the same as (3.60) - (3.65).

4) THE REDUNDANCY CONTRIBUTION:

The same as in Section 3.8.

For the convenience of practical implementation and better understanding of the proposed framework, an algorithmic flow is suggested in Fig. 4.1.

5. CONCLUDING REMARKS

This manuscript exhibited flexible algorithmic formulation for Kalman filtering with equality constraints on the system states, and practically developed an analytic framework for comprehensive error analysis accordingly. Specifically, this manuscript has:

 (a) Developed a unique formula set as an innovative framework on the base of the three independent error sources that influence the system state estimate (Section 3.1-3.6);



Fig. 4.1 an algorithmic flow of EKF with Constraints

- (b) Specifically introduced the equation for the residual vector of the process noise vector, as well as their covariance matrices (Section 3.6);
- (c) Made the reliability analysis feasible through parametrically introducing the redundancy contribution for the predicted state vector, process noise vector, and measurement vector, and the individual redundant indexes for the elements in the process noise and measurement vectors under the assumption of diagonal Q(k) and R(k) (Section 3.7); and
- (d) Pointed out its essential potentials how further algorithmic extension may be accomplished from the proposed formulation (Sections 3.9).

This work took an important step towards a standardized generic approach to performing Kalman filtering with equality constraints that enables comprehensive and rigorous error analysis, which is particularly important for high accuracy applications, for instance, the centimeter level kinematic positioning and navigation using GNSS and/or multisensor-integrated systems in the modern direct-georeferencing technology, autonomous vehicle driving, and other robotic applications etc., wherever it is important to examine the sources of any deviations in the estimated system states. The issue of comprehensive error analysis in Kalman filtering has been addressed previously [Wang, 1997; Caspary and Wang, 1998; Wang, et al, 2021; etc.], but not yet in the context of a Kalman filter with equality constraints. It is the authors' hope that comprehensive error analysis becomes a necessary part of the estimation process in the constrained Kalman filtering as a result of this work.

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Appendix: Proof of (3.24) and (3.25)

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$$\{ D_{xx}^{-1}(k) + C^{T}(k)R^{-1}(k)C(k) \}^{-1}$$

$$= \{ D_{xx}^{-1}(k/k-1) + C^{T}(k)R^{-1}(k)C(k) \}^{-1}$$

$$= D_{xx}(k/k-1) - D_{xx}(k/k-1)C^{T}(k)R^{-1}(k)C(k)D_{xx}(k/k-1)$$

$$= D_{xx}(k/k-1) - D_{xx}(k/k-1)C^{T}(k)D_{dd}^{-1}(k)C(k)D_{xx}(k/k-1)$$

$$= [E - D_{xx}(k/k-1)C^{T}(k)D_{dd}^{-1}(k)C(k)]D_{xx}(k/k-1)$$

$$= [E - K(k)C(k)]D_{xx}(k/k-1)$$

$$= D_{xx}(k/k)$$

$$D_{xx}^{-1}(k)X(k) = D_{xx}^{-1}(k)[(E - K(k)C(k))x(k/k-1) + K(k)z(k)]$$

$$= [C^{T}(k)R^{-1}(k)C(k) + D_{xx}^{-1}(k/k-1)][(E - K(k)C(k))x(k/k-1) + K(k)z(k)]$$

$$= C^{T}(k)R^{-1}(k)C(k)x(k/k-1) - C^{T}(k)R^{-1}(k)C(k)K(k)C(k)x(k/k-1) + D_{xx}^{-1}(k/k-1)x(k/k-1)$$

$$- D_{xx}^{-1}(k/k-1)K(k)C(k)x(k/k-1) + C^{T}(k)R^{-1}(k)C(k)K(k)z(k) + D_{xx}^{-1}(k/k-1)K(k)z(k)$$

$$= D_{xx}^{-1}(k/k-1)x(k/k-1) + C^{T}(k)R^{-1}(k)\{C(k)x(k/k-1) + t(k)-1\}$$

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